the undersigned at the number listed below.

Respectfully submitted,

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Enclosure: Appendix I (Marked-Up Version of Amended Specification)
DC080576

APPENDIX I

MARKED-UP VERSION OF AMENDED SPECIFICATION

On Page 31, Paragraph 3:

If the multiplication factor converting directions of the anamorphic prism are such that $\beta 1 = \beta A \times \beta 2$, as described above, the shift of the focussing position with respect to the defocussing ΔDef is such that

direction 1: $\Delta 1 \fallingdotseq \Delta Def \times 2 \times (\beta A \times \beta 2)^2$

direction 2: $\Delta 2 \fallingdotseq \Delta Def \times 2 \times \beta 22\ \beta 2^2$.

On Page 31, Paragraph 4:

The spot diameter $\phi 1$ on focussing is given by

$$(Spp/2) \times 2 \times \{(\beta A \times \beta 2)^2 \times \{(2 \cdot NA)/(\beta A \times \beta 2)\}$$

$$= 2 \cdot NA \cdot Spp \cdot (\beta A \times \beta 2)$$

...(1).

On Page 32, Paragraph 1:

If, in the above equation 1, the focussing pull-in range Sp is fixed and the spot diameter $\phi 1$ on focussing is fixed, the spot diameter $\phi 1$ is given by

$$\phi \fallingdotseq 2 \cdot NA \cdot Spp \cdot (\beta A \times \beta 2) = \text{constant}$$

so that the multiplication factor $\beta 2$ for the direction 2 for detecting the tracking error and the land-groove discrimination signal is in proportion to $1/\beta A$.

~~1/βA.~~ β2∝1/βA

So, the variation of the spot diameter $\phi 2$ for the defocussing Δdef is

$$\Delta\phi 2/\Delta Def \fallingdotseq 4 \cdot NA \cdot \beta 2 \propto 1/\beta A \quad \cdots(3)$$

so that it is inversely proportional to the multiplication factor βA of the anamorphic prism. Meanwhile, if the direction of the multiplication factor of the anamorphic prism is the radial direction, it suffices to substitute $1/\beta A$ for βA.